

# Progress on 1.5m Aperture Telescope and Instruments: Solar UV, Visible and near IR Telescope (SUVIT)

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and Solar-C/Chromosphere sub-WG

# Solar Optical Telescope

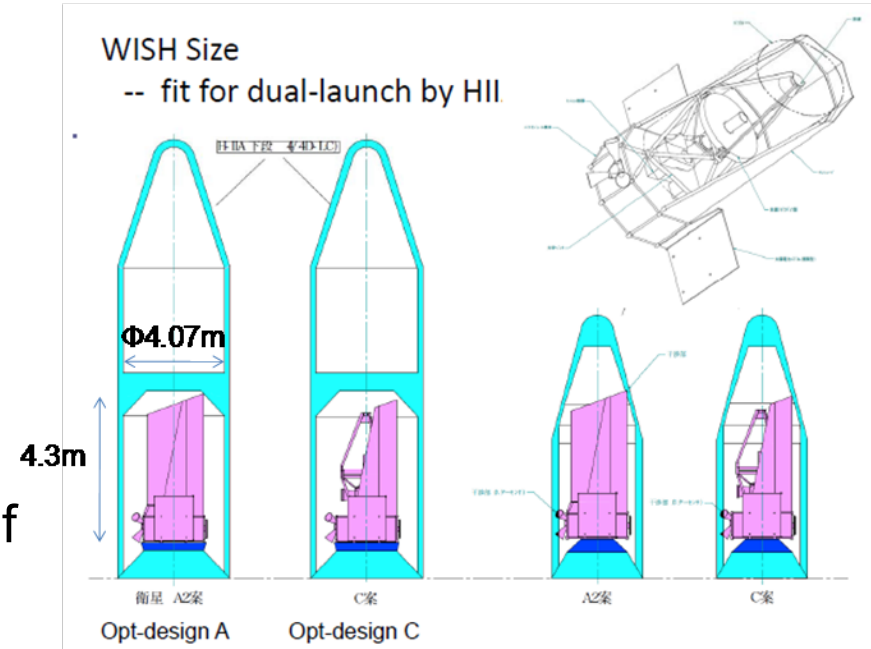
space	Ground -based
SOT $\Phi$ 1.5 m (planned 1980) resolve photon mean-free-path scale in the photosphere	
OSL $\Phi$ 0.8 m (planned late 1980s)	
Spacelab 0.3 m	
Hinode/SOT $\Phi$ 0.5 m (2006~) need more photons and resolution!	NST $\Phi$ 1.6 m (2009~) GREGOR $\Phi$ 1.5 m (2010?~)
Solar-C/Plan-B	ATST $\Phi$ 4 m (2018?~)

Heritage of developments of Hinode/SOT and large-aperture ground based telescope.

→ Technology is getting mature enough to build 1.5-m class space-borne telescope.

# Basic requirements to the instrument

- Telescope aperture and length
  - 1.5m $\phi$
  - Fit within the H-IIA nose fairing
- Spatial resolution
  - 0.1" in UV
  - 0.16" in Vis/NIR (Diffraction limit of 1.5m $\phi$  at 1 $\mu$ m )
- FOV
  - ~200" x 200" to cover a medium size AR with 4kx4k detector
- Wavelength coverage (250 – 1100 nm)
  - Shortest ~250 nm to observe Mg II h/k.
  - Longest ~1100 nm to observe He I 10830.
- I/F between the telescope and the focal-plane instrument
  - Collimated beam with ~ $\phi$ 60mm exit pupil to relax the tolerance of alignment.



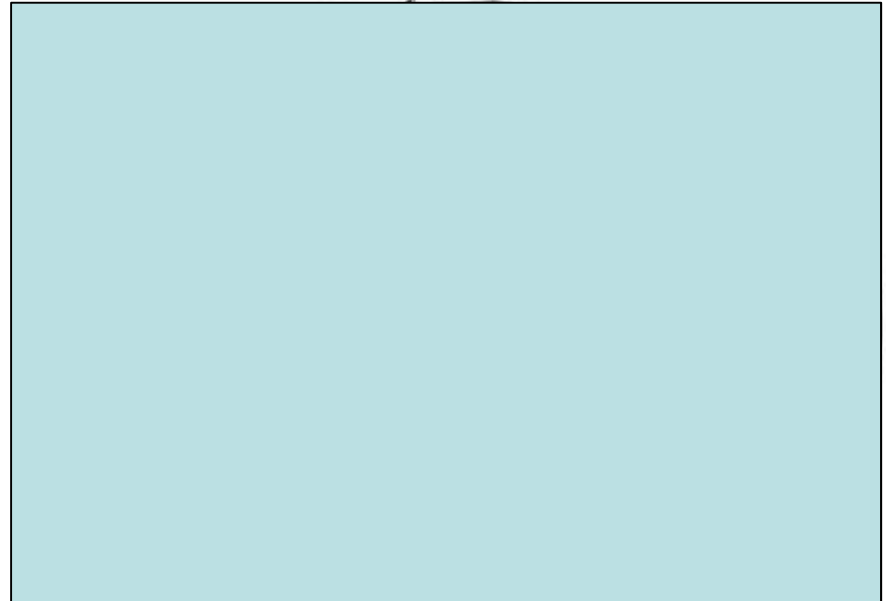
# Primary Mirror

Monolithic light-weight mirror for 1-1.5 m aperture are feasible

- 90% light-weighting: 100 – 150 kg (weight budget)
- Small gravity effect in horizontal configuration
  - WFE < 35 nm rms (optical performance)
  - coma < 4 nm rms (alignment)

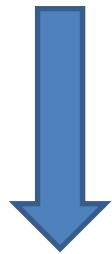
Coating chamber can be accommodated with 1.5 m mirror

Structure model of the Sunrise 1-m aperture primary

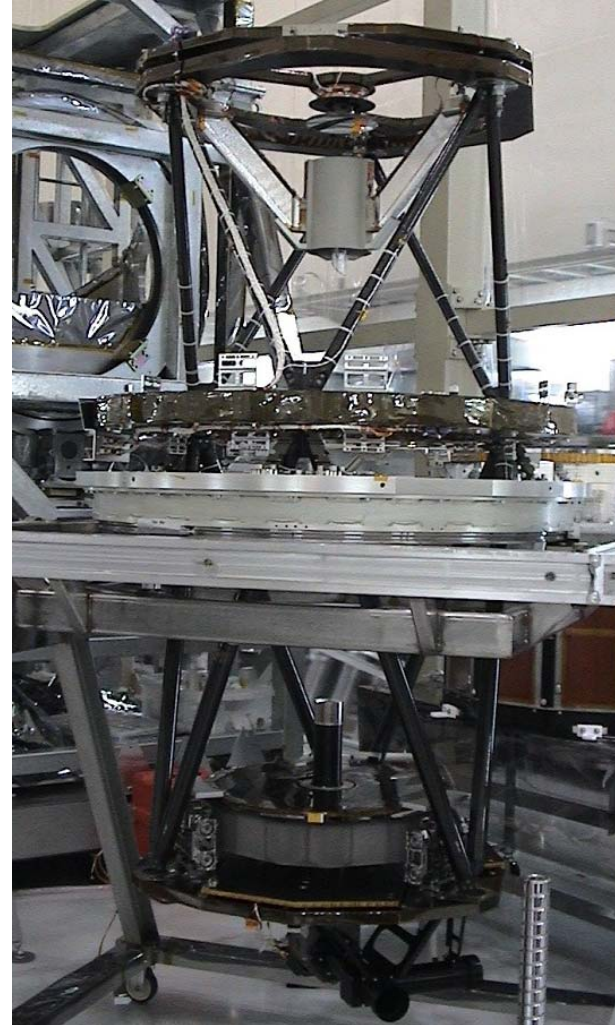


# Telescope Structure

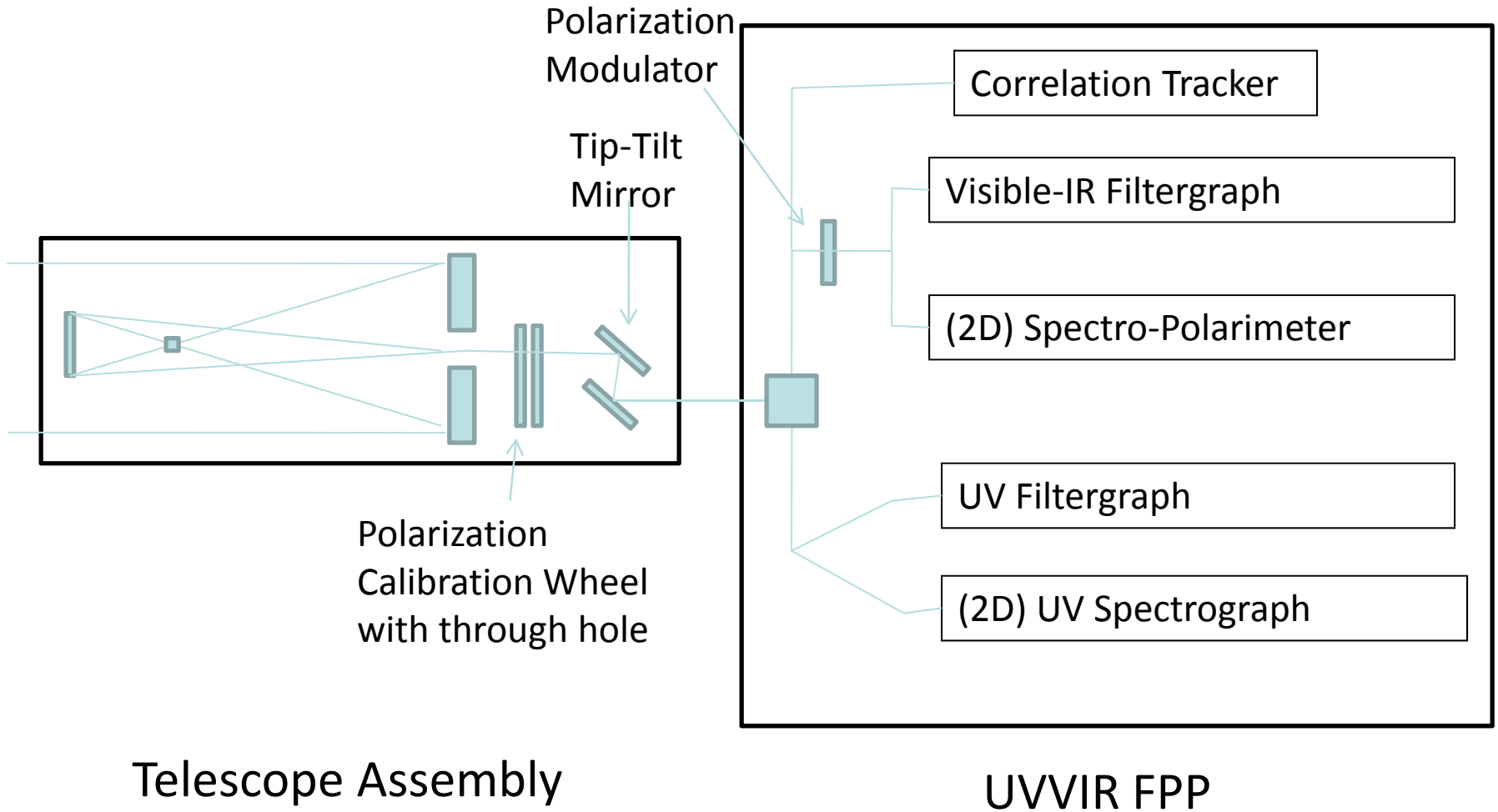
Hinode/SOT truss structure of CFRP (CTE < 0.1 ppm/K)



Thermal stability ( $\Delta T=5$  deg) in focus accommodate 1.5 m aperture and 3 m M1-M2 length Gregorian.



# Conceptual Design for SUVIT



# Positional Tolerance Study of $\phi 1.5$ m Gregorian

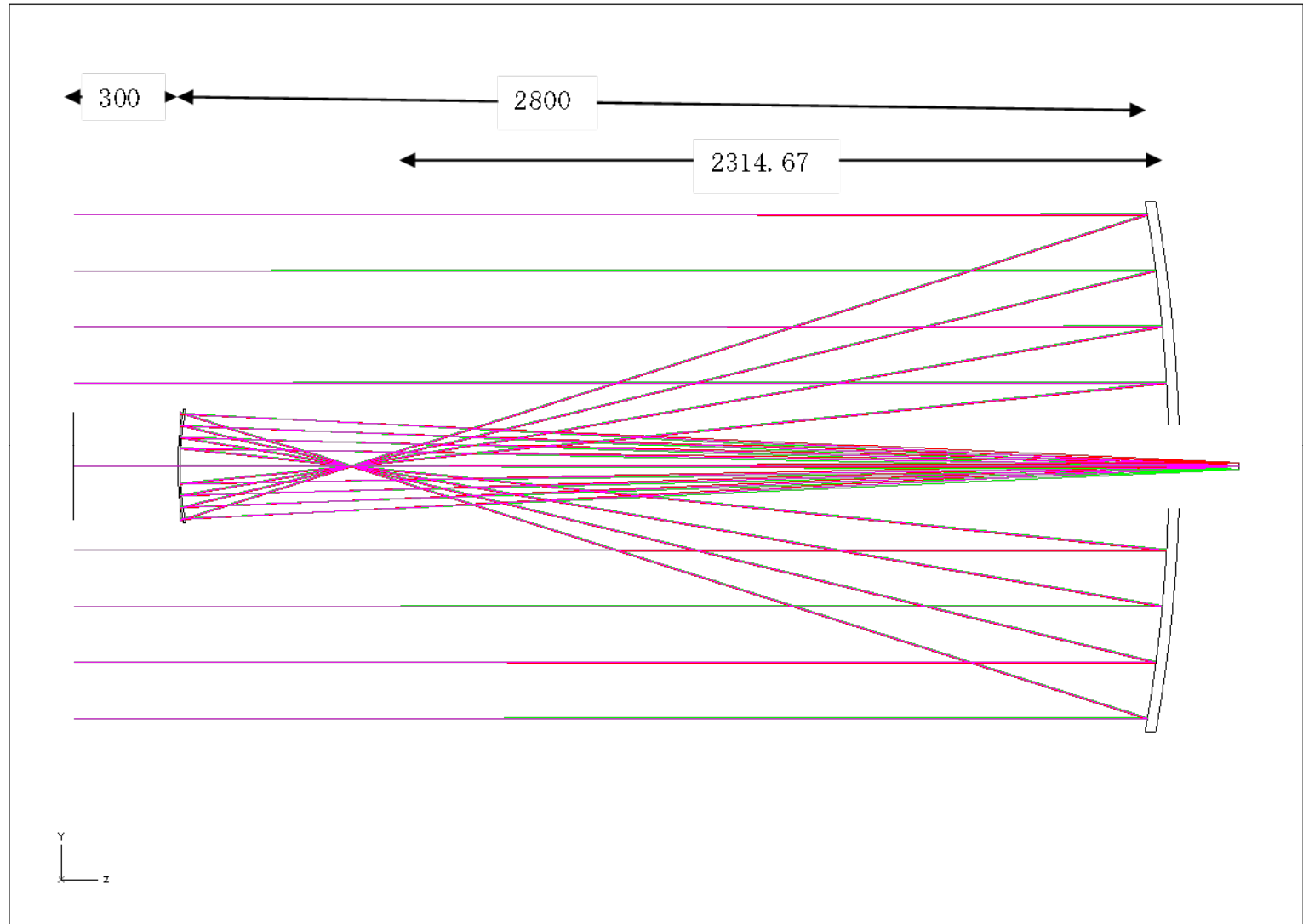
M1-M2 (cm)	300	280	250	220	OTA 150
f1 (cm)	246.6 (F1/1.64)	231.467 (F1/1.54)	208.467 (F1/1.39)	185.167 (F1/1.23)	116.9617 (F1/2.34)
f2 (cm)	45.7633	41.775	35.9961	30.4184	26.247
Defocus $1\ \mu$ A20 (Strehl)	0.0367 (0.983)	0.0415 (0.980)	0.0508 (0.968)	0.0636 (0.951)	0.0178 (0.997)
Defocus $3\ \mu$ A20		0.1245 (0.832)	0.1522 (0.748)		0.057 (0.967)
Decenter $10\ \mu$ A31	-0.0359 (0.994)	-0.0432 (0.991)	-0.0588 (0.983)	-0.0831 (0.966)	-0.0125 (0.999)
Decenter $50\ \mu$ A31		-0.216 (0.791)	-0.294 (0.653)	-0.4156 (0.4267)	-0.0625 (0.98)
Tilt $10''$ B31	0.0908 (0.960)	0.0996 (0.952)	0.1161 (0.936)	0.1379 (0.910)	0.01897 (0.998)
Tilt $50''$ B31	0.454 (0.362)	0.498 (0.289)	0.581 (0.190)		0.0948 (0.955)

# Baseline Optical Parameters

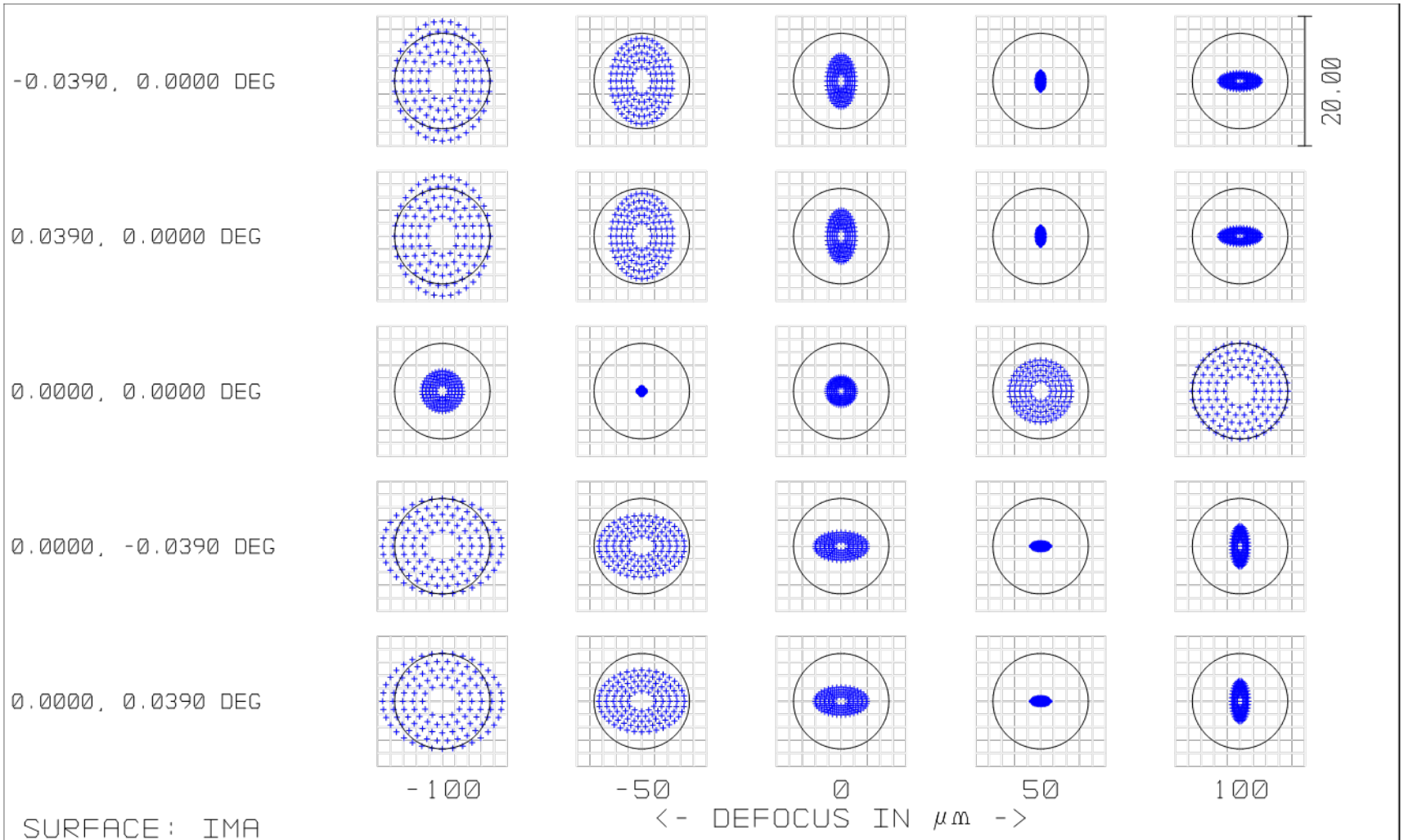
	SOT-OTA (SOLAR-B)	SUVIRT-OTA (SOLAR-C)
Entrance pupil (mm)	500	1500
M1-M2 distance (mm)	1500	2800 (<4500)
M1 outer diameter (mm)	560	1580
clear aperture	509	1513
radius (focal)	2339.4 (1169.7)	4629.34 (2314.67)
conic const.	-0.9706	-0.990927
M2 outer diameter (mm)	159	340
clear aperture	147	320.5
radius (focal)	524.94 (262.47)	835.494 (417.747)
conic const.	-0.3996	-0.548155
HDM outer diameter (mm)	32.83	48.37



# Baseline Telescope Design



# Spot Diagram



## THROUGH FOCUS SPOT DIAGRAM

SOLAR-C GREGORIAN G3  
 THU OCT 8 2009 UNITS ARE  $\mu\text{m}$ . AIRY RADIUS : 7.364  $\mu\text{m}$   
 FIELD : 1 2 3 4 5  
 RMS RADIUS : 2.478 2.478 1.703 2.478 2.478  
 GEO RADIUS : 3.981 3.981 2.155 3.981 3.981  
 SCALE BAR : 20 REFERENCE : CHIEF RAY

GREG\_G3\_2800.ZMX  
 CONFIGURATION 1 OF 10

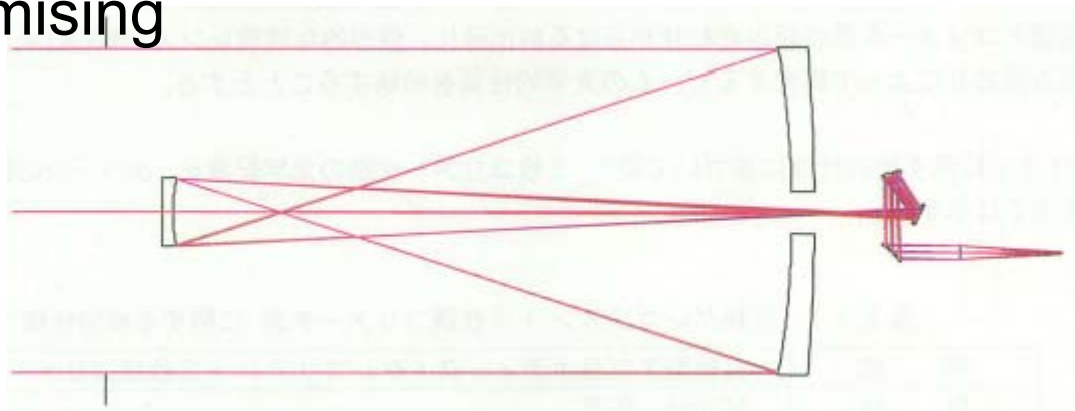
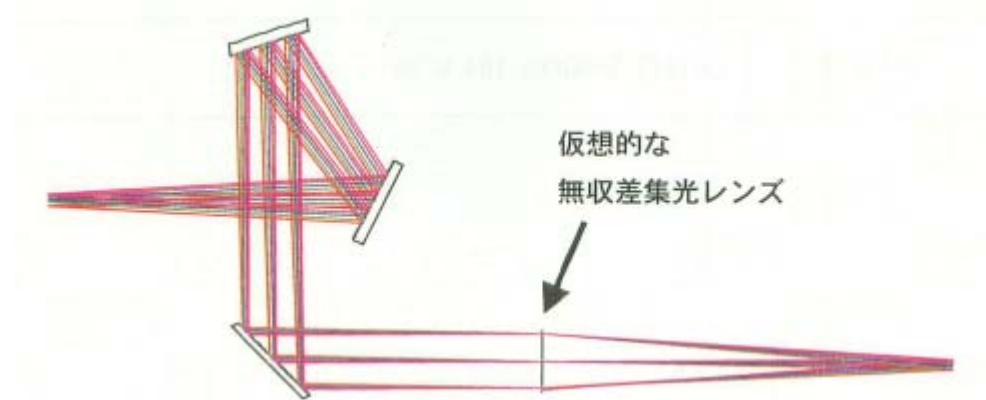
# Collimating Optics

Trade off study among

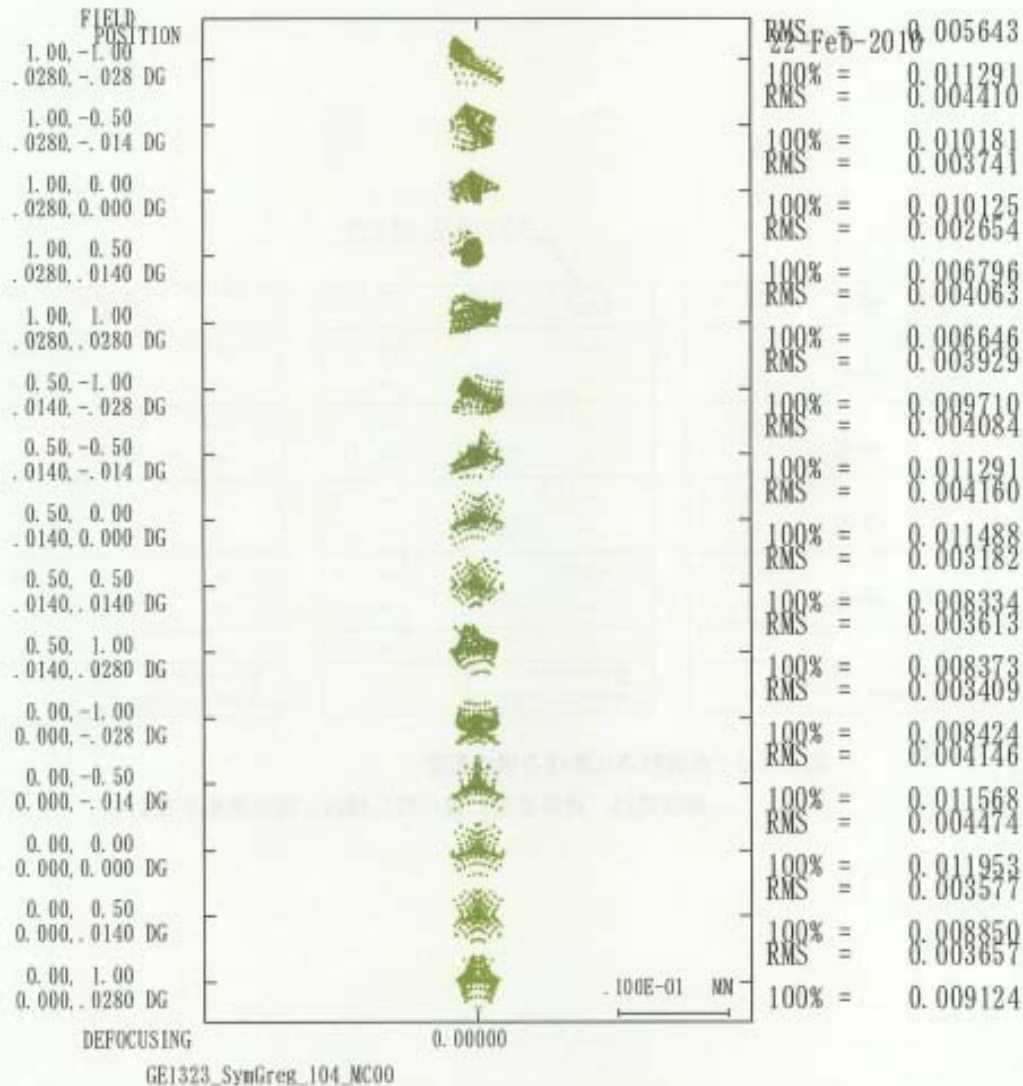
1. All reflective
2. Lens (SiO<sub>2</sub>, CaF<sub>2</sub>)
3. Composite lens-Cassegrain design

- Chromatic aberration
- Thermal stability in focus

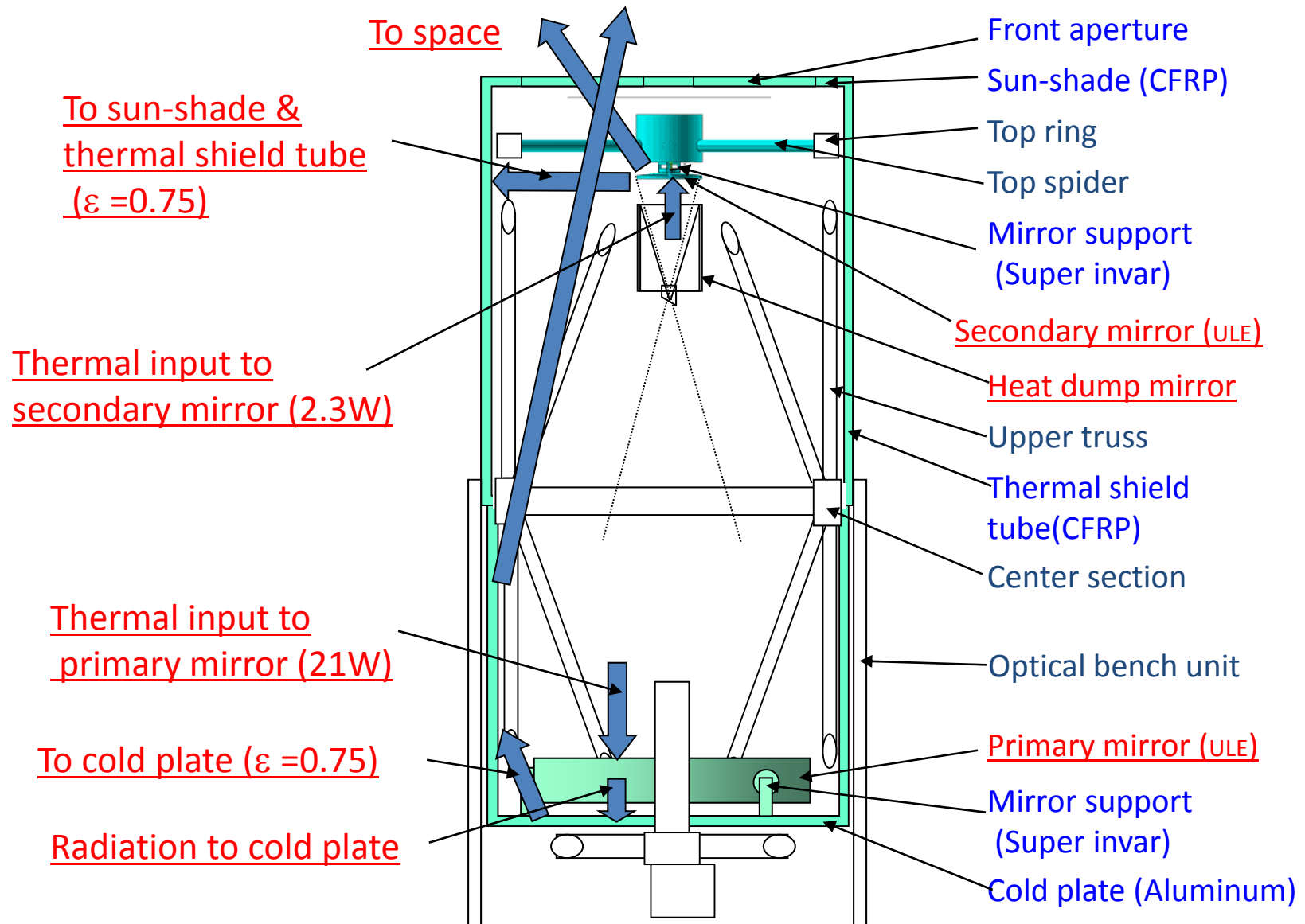
All reflective option is promising



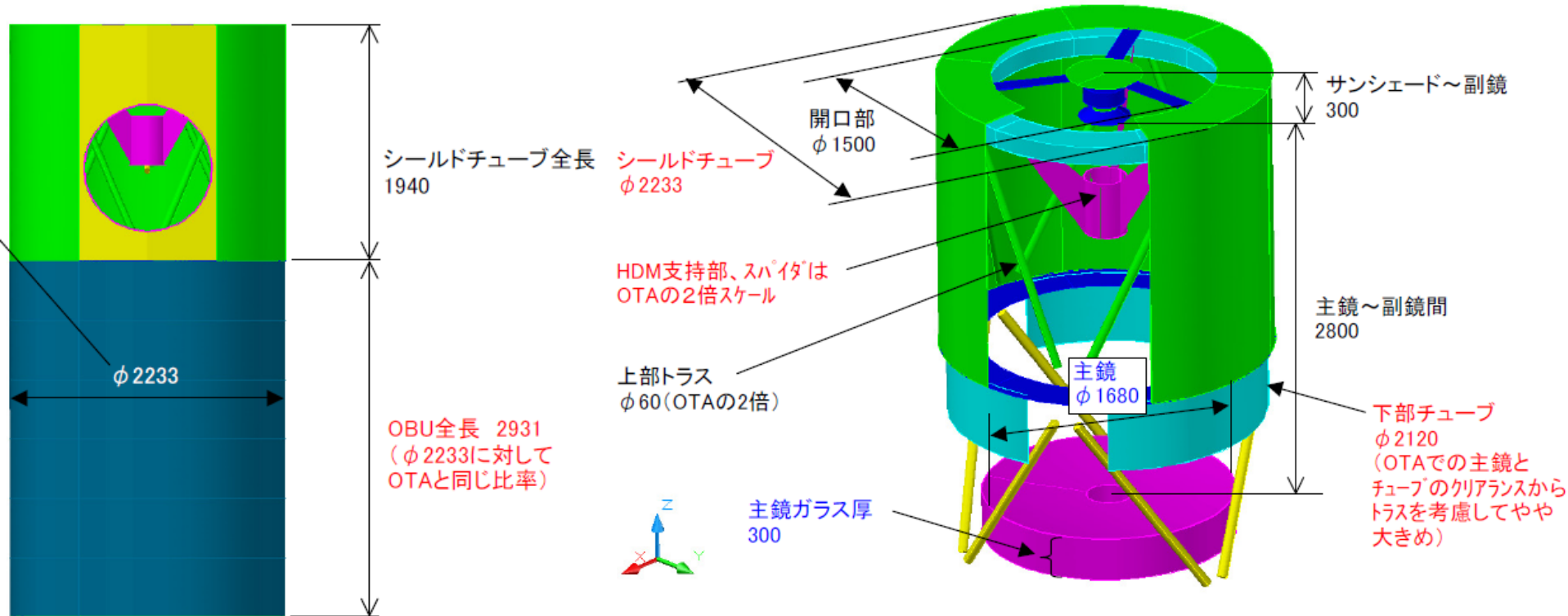
# Spot diagram for Gregorian + 3-mirror collimator



# Heat dump path from M1 and M2 in case of Solar-B OTA



# Structure Model of $\phi 1.5$ m Telescope: Scaled-up model of OTA



**Thermal properties of surfaces are of end-of-life except for M1 and M2.**

名称	吸収率 $\alpha$		入射量(W)	吸収量(W)
主鏡	$\alpha 1$	0.118	2074.9	244.8
排熱鏡	$\alpha H$	0.1	1830.1	175.4
副鏡	$\alpha 2$	0.118	76.2	9.0
コリメータ	$\alpha 3$	0.11	19.4	2.1
合計				431.4

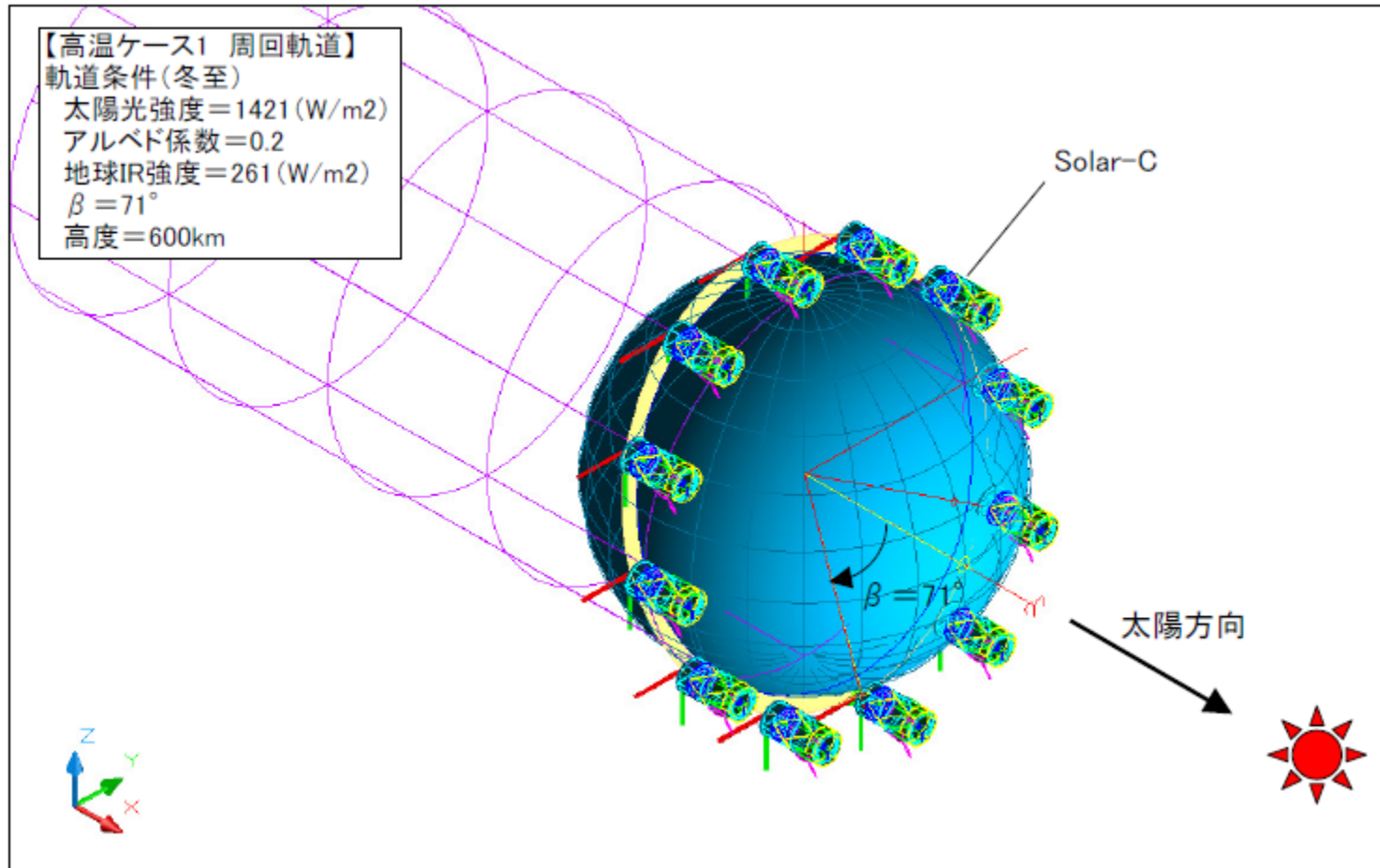
改訂

OTA	$\alpha$	OTA吸収量(W)
	0.1	22.3
	0.15	27.2
	0.1	2
	TBD	0.5
合計		52

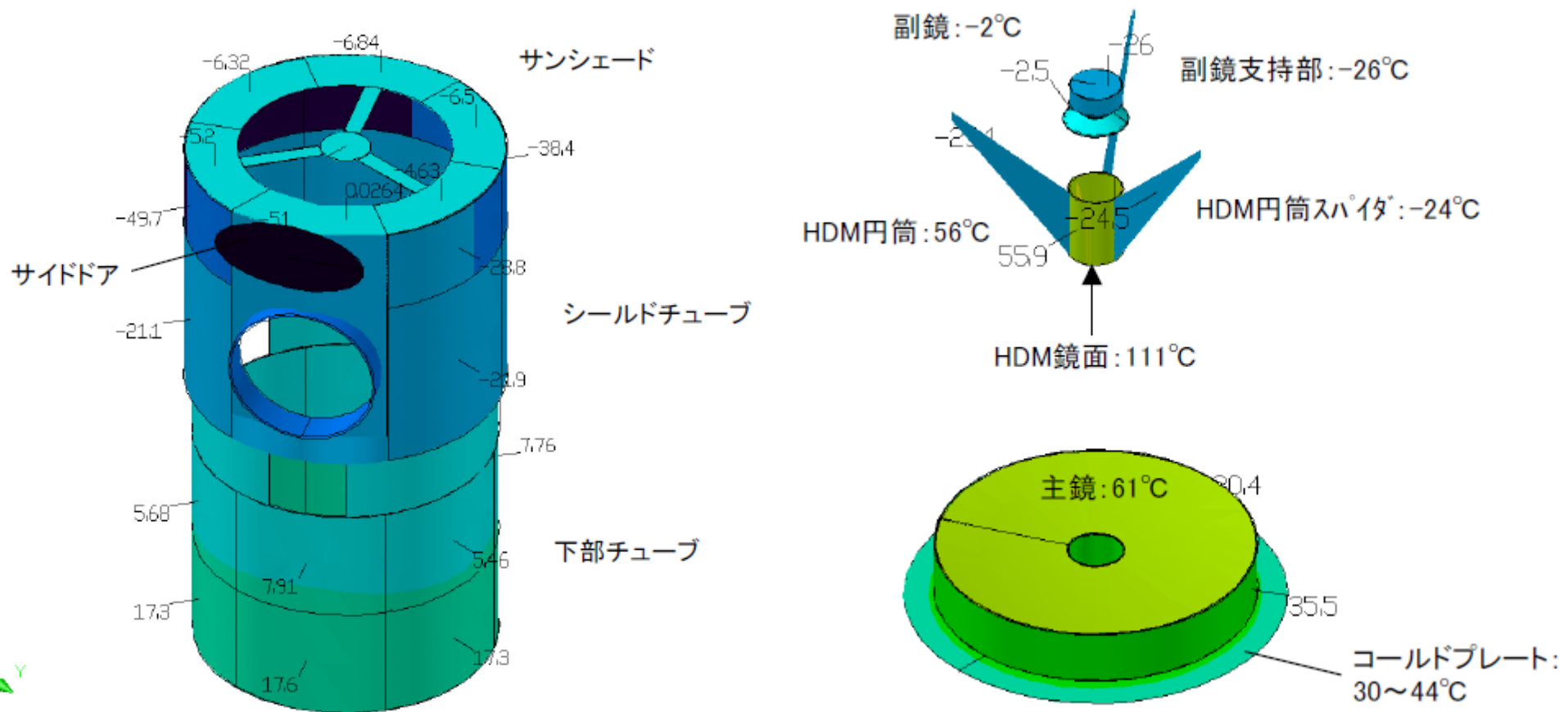
※  $\alpha$  の値はICDパッケージより抜粋(中間報告と異なる)

※ OTA熱設計中間報告より

# Solar-C Solar Synchronous Polar Orbit same as Hinode

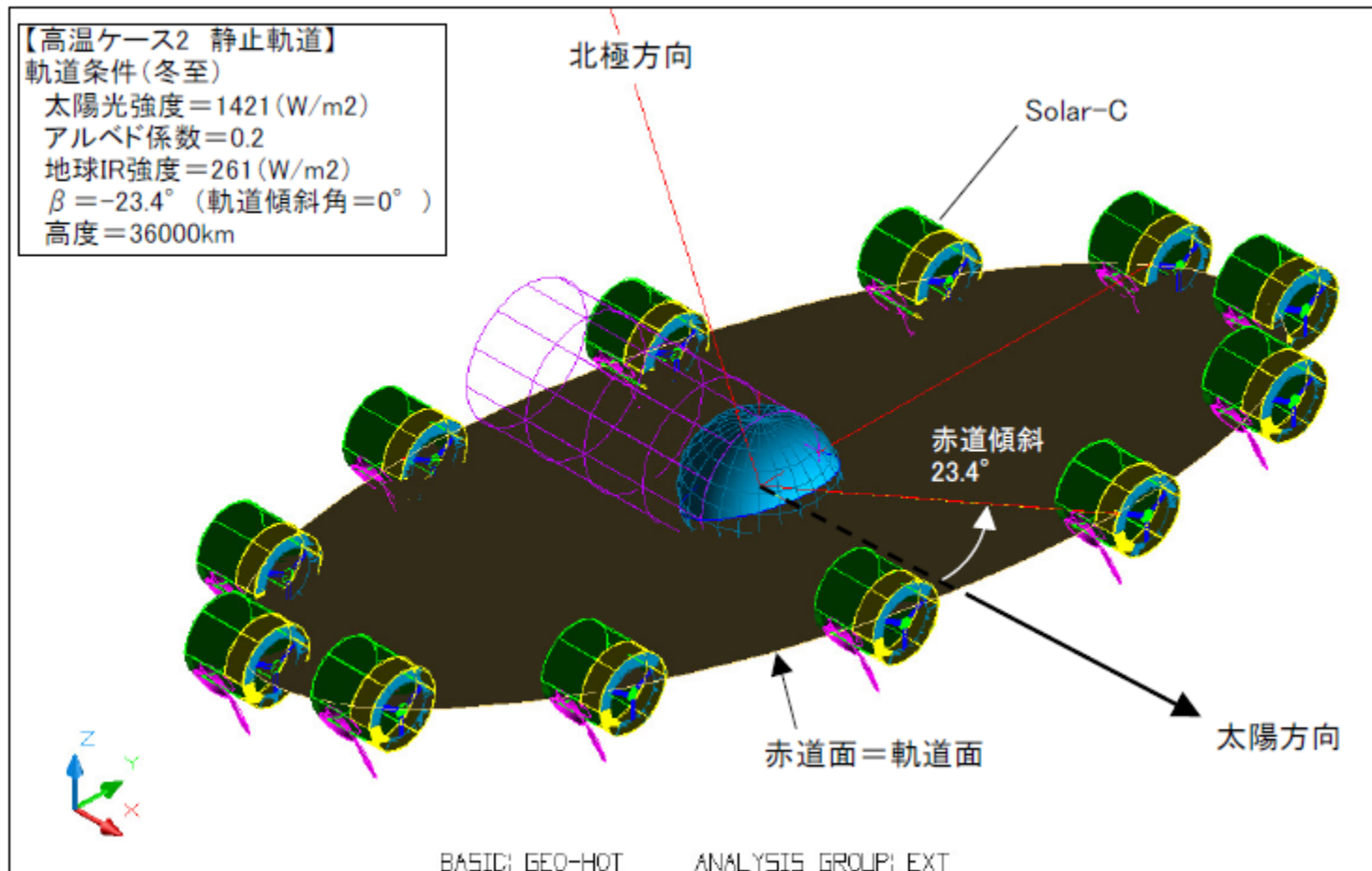


# Temperatures for Polar Orbit

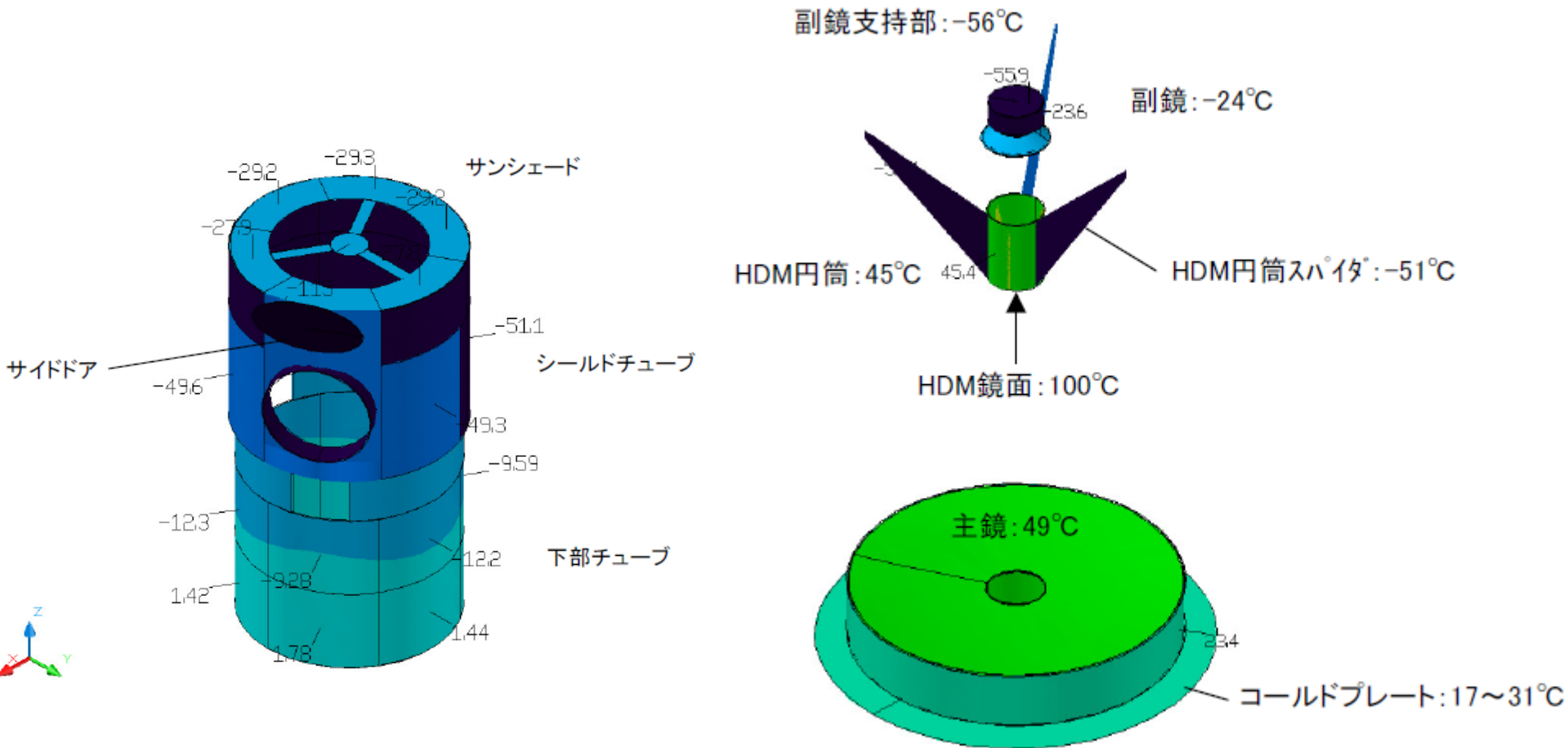




# Solar-C Geosynchronous Orbit

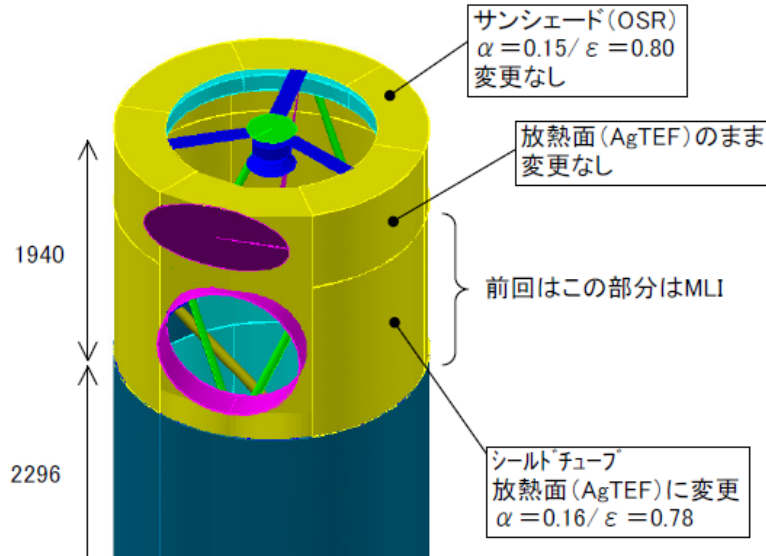


# Temperatures for Geosynchronous Orbit



# Sensitivity study with radiator area modification

## 1) Mod-1 Expand radiator area at Shield Tube



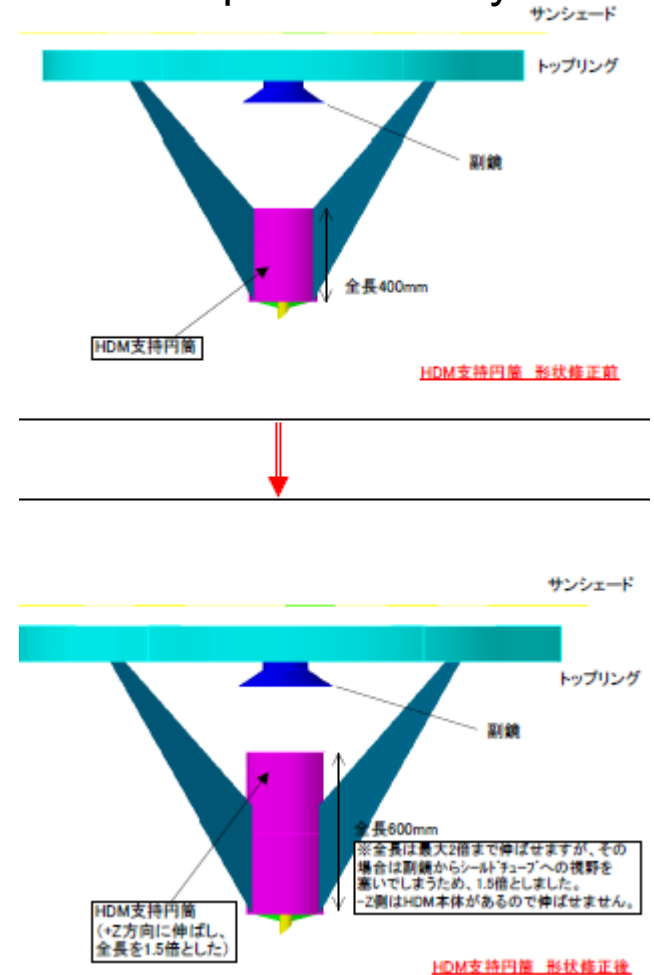
## 2) Mod-2 Enhance conduction at HDM inner spider

AlBe (210W/mK) x 3 spiders



AlBe (210W/mK) x 6 spiders

## 3) Mod-3 Expand HDM cylinder

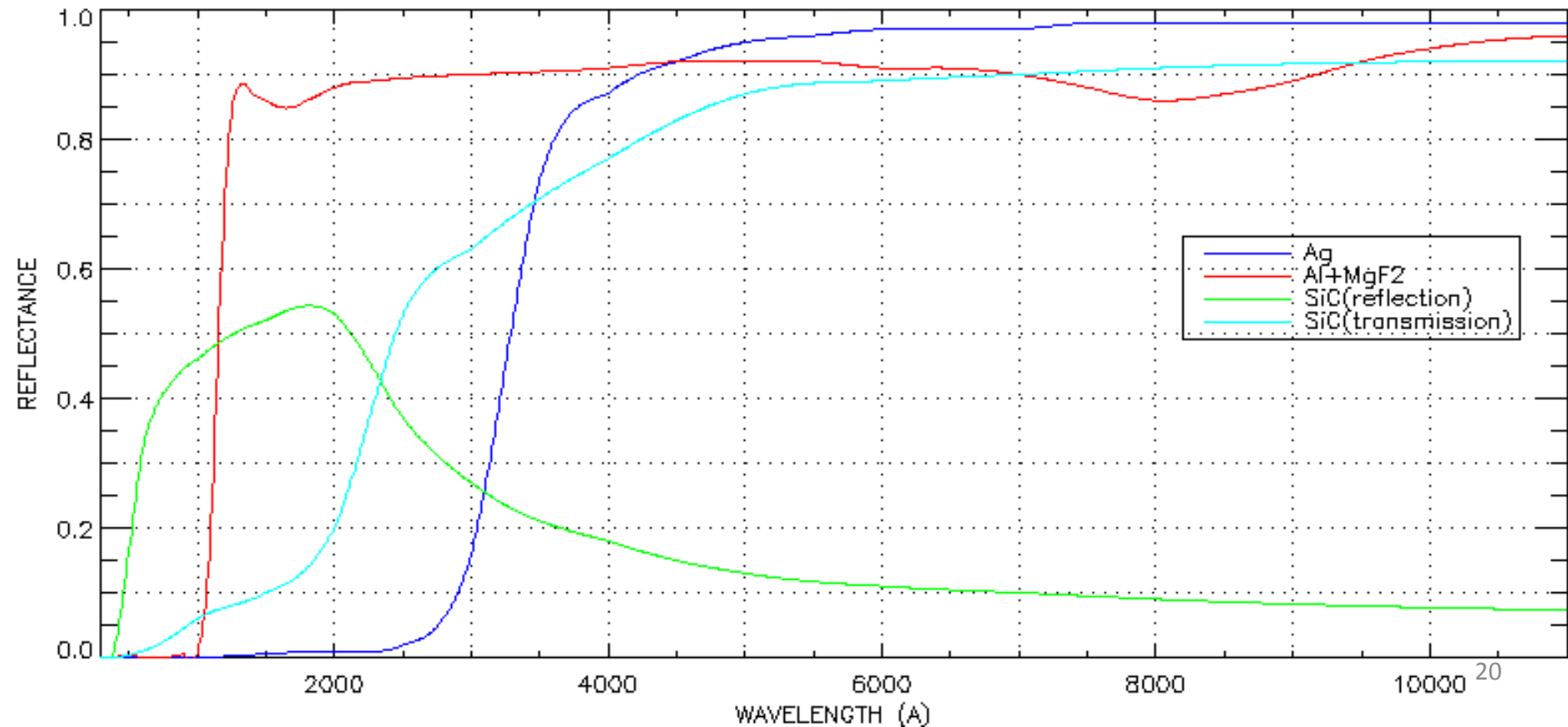


# Mirror Coating Issue

Hinode/OTA: M1 and M2 have a protected Ag coat (solar light absorption  $\alpha \sim 6.5\%$ ) which is not suitable for UV observation (not capable of reflecting UV light shorter than 360 nm).

A typical coating for UV is Al+MgF<sub>2</sub>. However, The coating has a large  $\alpha$  of  $\sim 12\%$  and overall reflectivity in visible and IR is Lower than the Ag coating.

→ The development of UV-reflective and low solar absorption coating is under study.



# Degraded (EOL) Reflectivity for Al+MgF2 Coating

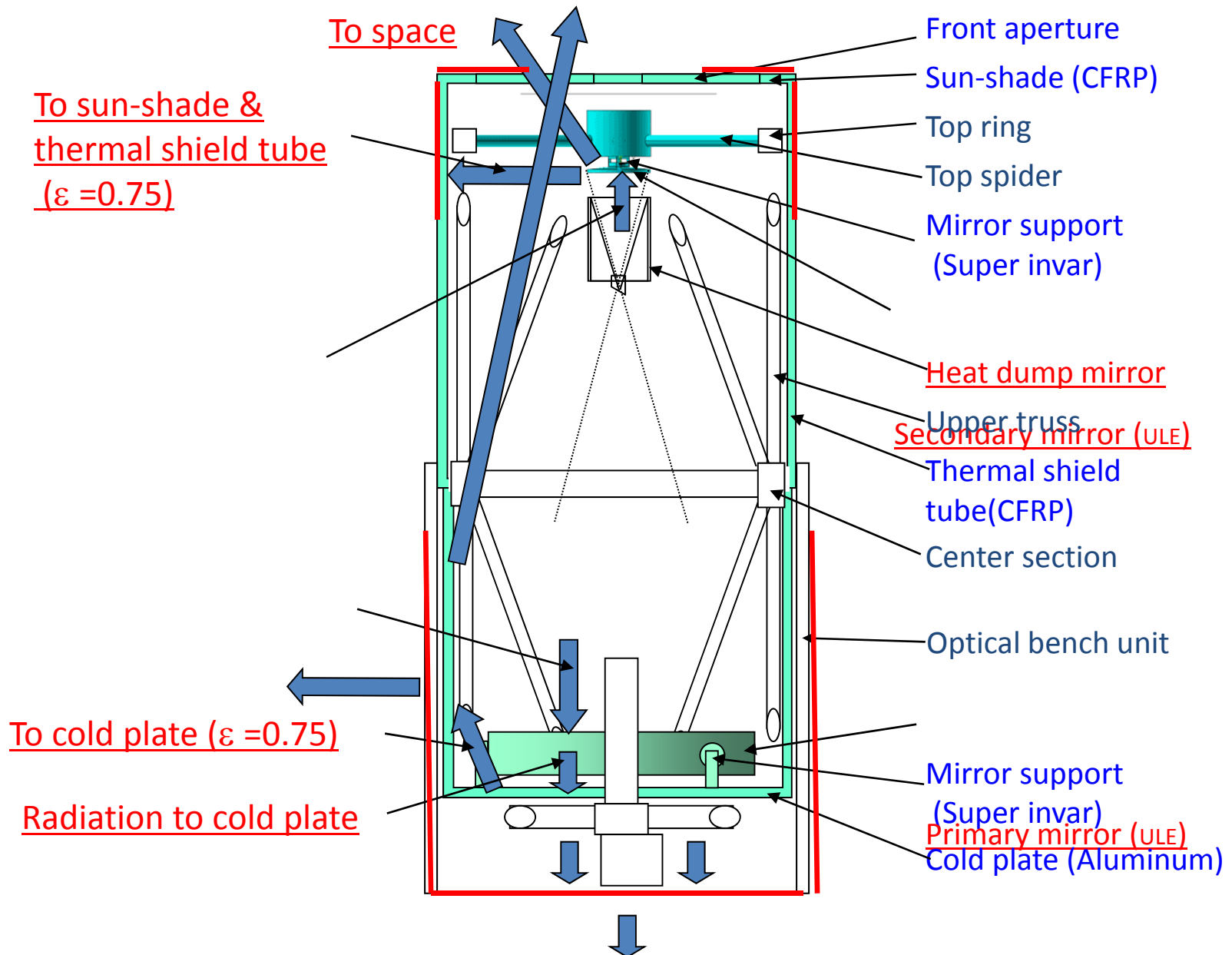
Assume that the solar absorption  $\alpha$  increase by 0.05 in the end of life (EOL).

名称	吸収率 $\alpha$		入射量(W)	吸収量(W)	変更前
主鏡	$\alpha 1$	0.168	2074.9	348.6	245
排熱鏡	$\alpha H$	0.1	1726.3	165.4	175
副鏡	$\alpha 2$	0.168	71.9	12.1	9
コリメータ	$\alpha 3$	0.11	18.6	2.0	2.1
合計				528.2	431

# Predicted temperatures for optics

T (degC)	Polar orbit	Geosyn c. orbit	Polar orbit with Mod-1	Polar orbit with Mdd-1 and Mod-2	Polar orbit with Mod-1 and Md-2 and Mod-3	Polar orbit +Mod-1 $\alpha+0.05$ @M1&M2	Geosync +Mod-1 $\alpha+0.05$ @M1&M2
M1 surface	61	49	52	52	52	80	70
M2 Surface	-2 ~ -7	-24	-12 ~ -8	-12 ~ -8	-12 ~ -7	0 ~ 4	-17 ~ -16
HDM surface	109 ~ 111	100	103 ~ 104	77 ~ 78	60 ~ 61	63 ~ 64	51
CLU	34 - 37	22-24	24 - 27	24 - 27	24 - 26	41	29

# Heat dump path from M1 necessary



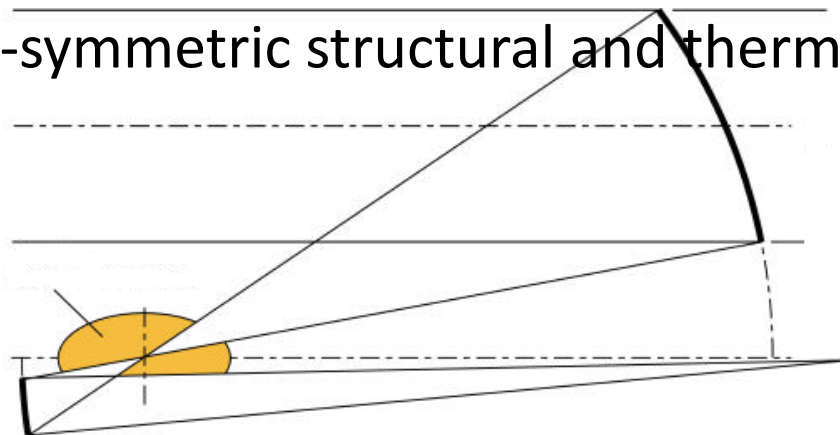
# Off-axis Gregorian

## Pro

- no central obscuration, lower scattered light, higher contrast images
- more freedom in designing HDM at primary focus, direction of reflected light and cooling method

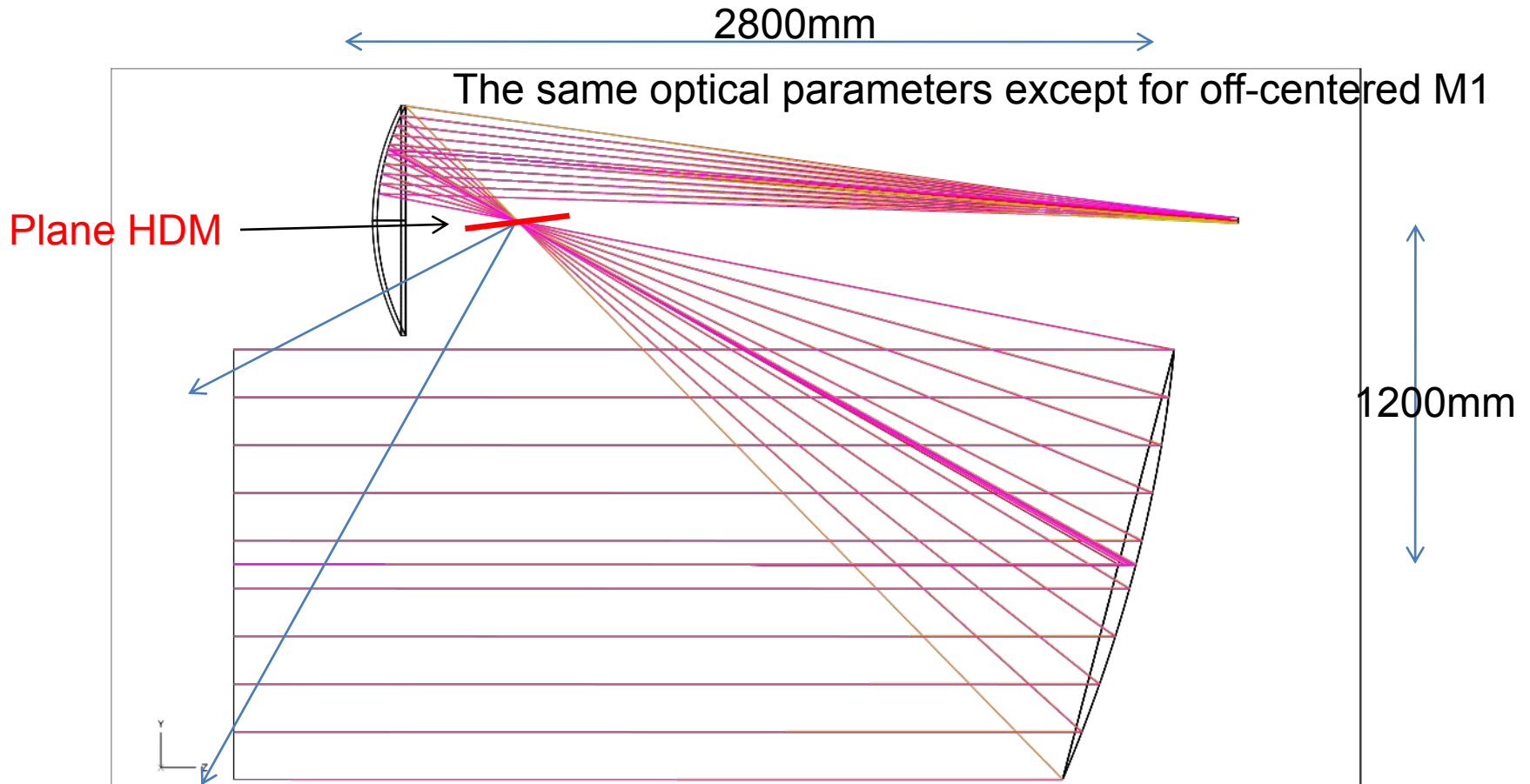
## Con

- larger instrumental polarization (may be calibrated with continuum and sunspot obs.)
  - harder to fabricate and validate M1 and M2 mirrors
- alignment
- higher non axi-symmetric structural and thermal deformation of telescope





# Off-Axis Gregorian



3D LAYOUT

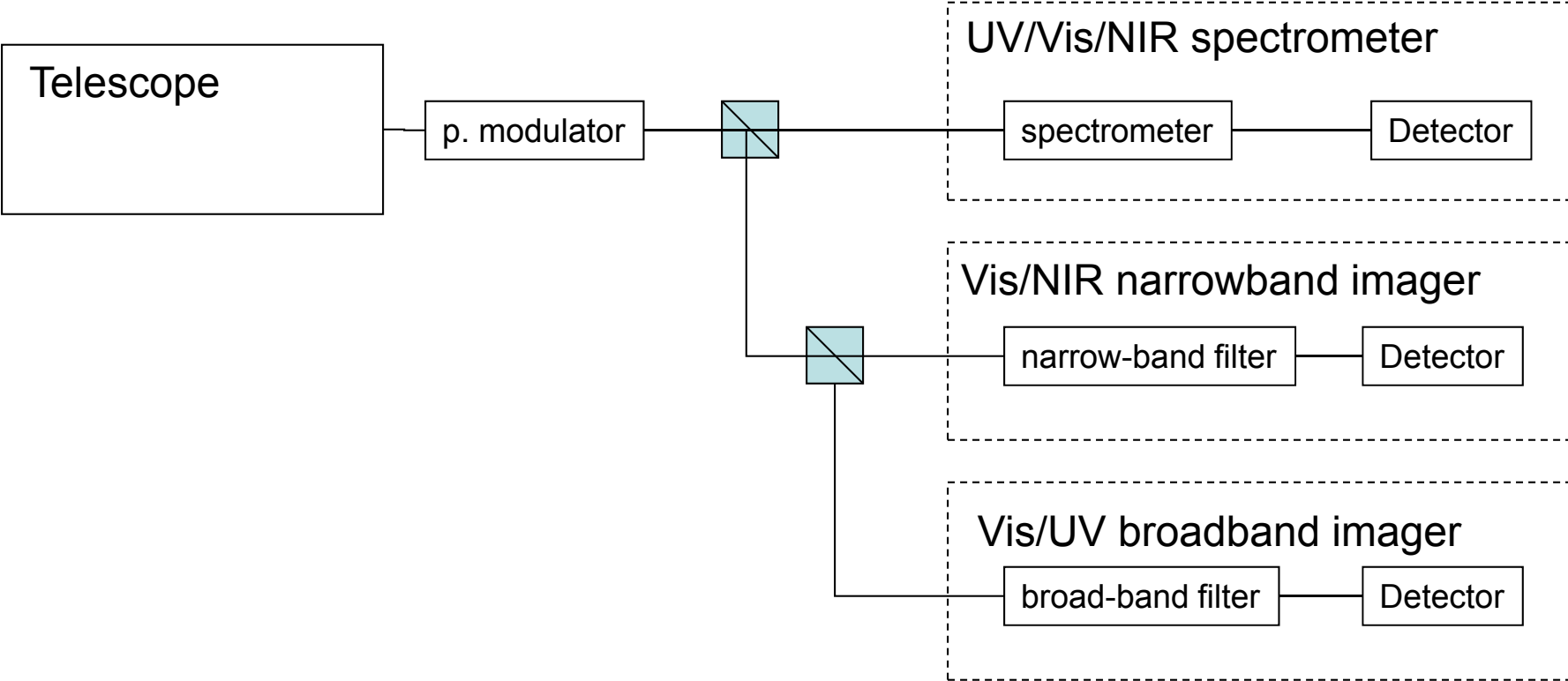
OFF-AXIS PARABOLA FOR UNOBSCURED GREGORIAN  
THU OCT 8 2009

OFF-AXIS\_GREG2800\_1000.ZMX  
CONFIGURATION 1 OF 1

# Preliminary choices of spectrum lines (most deluxe configuration)

Instrument	Spectrum line	wavelength	Purpose
Vis/UV broadband imager	UV continuum	~250nm	High res. Img of photosphere
	Mg II h/k	280nm	High res img of chromosphere
	CN band	388nm	Granules and magnetic elements
	<i>G-band</i>	<i>430nm</i>	<i>Granules and magnetic elements</i>
Vis/NIR narrowband imager  +He D3	Mg Ib2	512nm	Low chromosphere V and B
	Fe I	525nm	Photosphere B
	Na ID1 (D2)	589nm	Low chromosphere V and B High photosphere
	H $\alpha$	656nm	High chromosphere V
	Ca II IRT	854nm	High chromosphere T, V and B
UV/Vis/NIR spectrometer  +Ca II IRT weaker line	Mg II h/k	280nm	High chromosphere T and V
	Ca II IRT	854nm	High chromosphere T, V and B
	He I	1083nm	High chromosphere V and B

# Block diagram of the optical configuration



## Pixel size and FOV of the instruments

		FOV	Pixel size	Exposure	Note.
UV-Vis-NIR telescope	Broad band	164" x 164"	0.04"	< 1sec	<ul style="list-style-type: none"> <li>• 2.5 pix sampling of <b>0.1"</b> res.</li> <li>• 4Kx4K detector</li> </ul>
	Narrow band	246" x 246"	0.06"	< 1sec	<ul style="list-style-type: none"> <li>• 2.5 pix sampling of <b>0.16"</b> res.</li> <li>• 4Kx4K detector</li> </ul>
	Spectrometer	246" x 246"	0.06"	1sec (S/N~1600)	<ul style="list-style-type: none"> <li>• 2.5 pix sampling of <b>0.16"</b> res.</li> <li>• 4K pix along slit</li> </ul>
0.12"			10sec (S/N~10 <sup>4</sup> )		

# Basic requirements on TF (preliminarily)

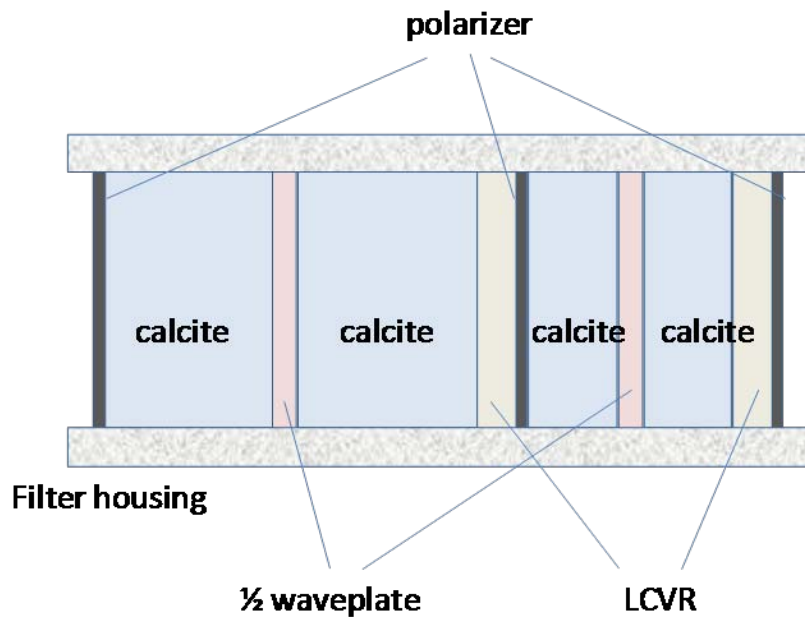
- Wavelength range TBD (a possibility 5000 – 8700Å)
- band width (FWHM) ~100mÅ (50~70mÅ)
- Strehl >0.9
- FOV ~200 arcsec w/ $\phi$ 1.5m (TBR)
- free spectral range >5Å
- tuning range +/- 5Å
- tuning speed <50ms
- tuning resolution <5mÅ
- repeatability <2mÅ
- uniformity
  - wavelength 5mÅ (TBD)
  - transmission 5%
- stability
  - wavelength 5mÅ /day
  - transmission (flat) 1% /day
- Parastic light <2%
- Ghost <1%
-

# Choice of tunable filter

Lyot filter

vs.

Fabry Perot



Need Bubble-free design!  
All elements can be attached with  
index matching oil?.

	Lyot filter	Fabry Perot
F (Speed of incident beam)	F~ 40	F ~ 200 (air space) ~ 90 (LiNb)
Necessary diameter of filter (D=1m, FOV=3')	~40mm	~180mm, ~80mm
Transmission	~ 5%	~ 70%
Simultaneous 2-polarization	impossible	possible
Simultaneous multi wavelen	(in principle possible)	impossible
Structure	Complex	High accuracy
Oil	Necessary	Free
Control device	Rot. waveplate or liquid crystal	Piezo or LiNb
Past experience	SOT/Hinode	LASCO C1/SoHO
Concern	<ul style="list-style-type: none"> <li>- Contact of opt. elem.s (avoiding bubble)</li> <li>- Mounting calcites</li> <li>- Outgas</li> <li>- Calcite availability</li> </ul>	<ul style="list-style-type: none"> <li>- Mount and control for high accuracy surfaces (thermal/mech. stress)</li> <li>- Endurance of coaring</li> <li>- Stability of inhomogeneity</li> </ul>

Filter diameter,  $L_{min} = \text{image size} = F * D * (W/60/180 * \pi) = 0.0003 * F * D * W$  (cm, Telecentric)  
D: aperture, cm、 W: FOV, arcmin、 F: F-ratio

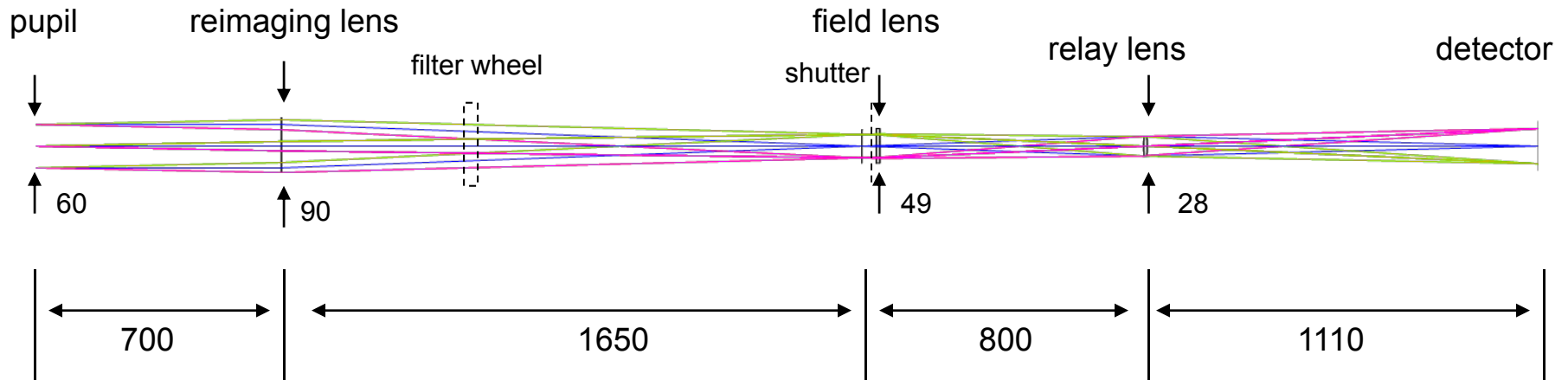
# Need of 2-dimensional spectroscopy

- Rapid motion of chromospheric materials are ubiquitously seen associated with eruptions, jets, and wave propagation.
- There are several options under investigation to achieve the 2D spectroscopy in SOLAR-C.
  - Double pass spectrograph
    - Slot spectroscopy with medium wavelength dispersion
  - Tunable filter-type instruments with rapid wavelength tuning
    - Fabry-Perot or Lyot
  - Integral field spectroscopy
    - Fiber-optics bundle or image slicer



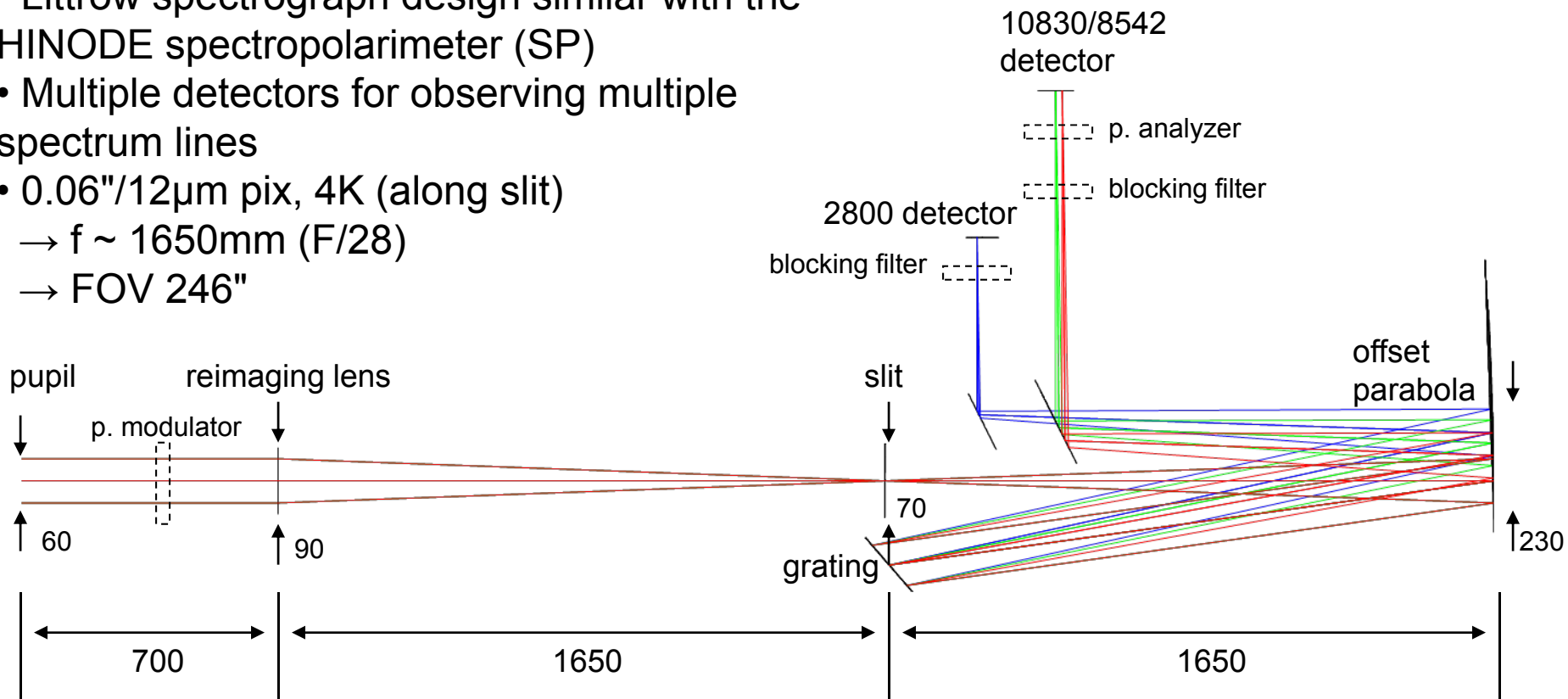
# Broadband imager layout

- Similar design with the HINODE broadband filter imager (BFI).
- The rotating shutter is located near the focal plane
- $0.04''/12\mu\text{m}$  pix,  $4\text{K}\times 4\text{K}$ 
  - $f \sim 2470\text{mm}$  (F/41)
  - FOV  $164''$



# Spectrograph layout

- Littrow spectrograph design similar with the HINODE spectropolarimeter (SP)
- Multiple detectors for observing multiple spectrum lines
- 0.06"/12 $\mu$ m pix, 4K (along slit)
  - $f \sim 1650$ mm (F/28)
  - FOV 246"

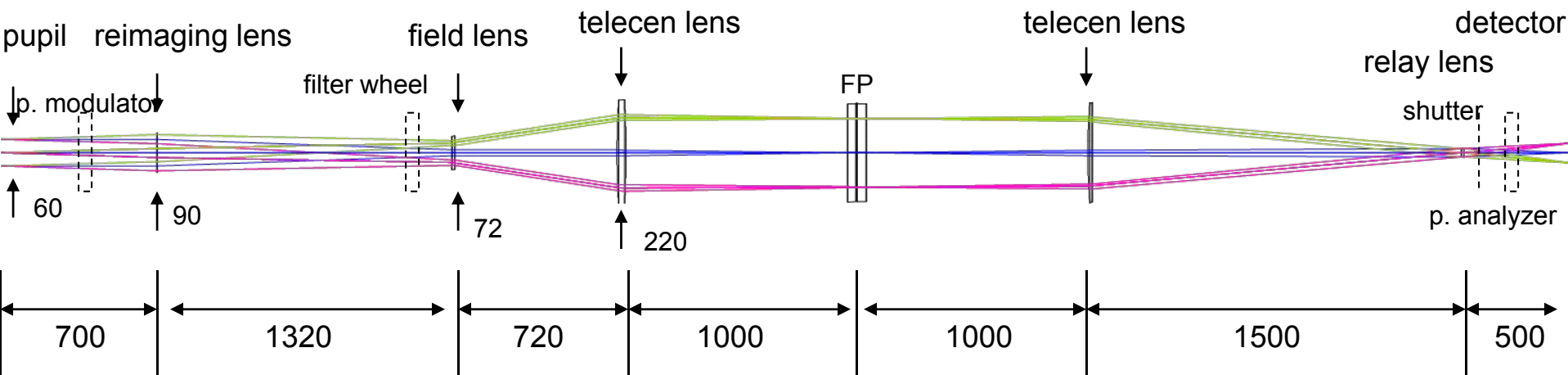


blaze angle	56°
groove	80lines/mm

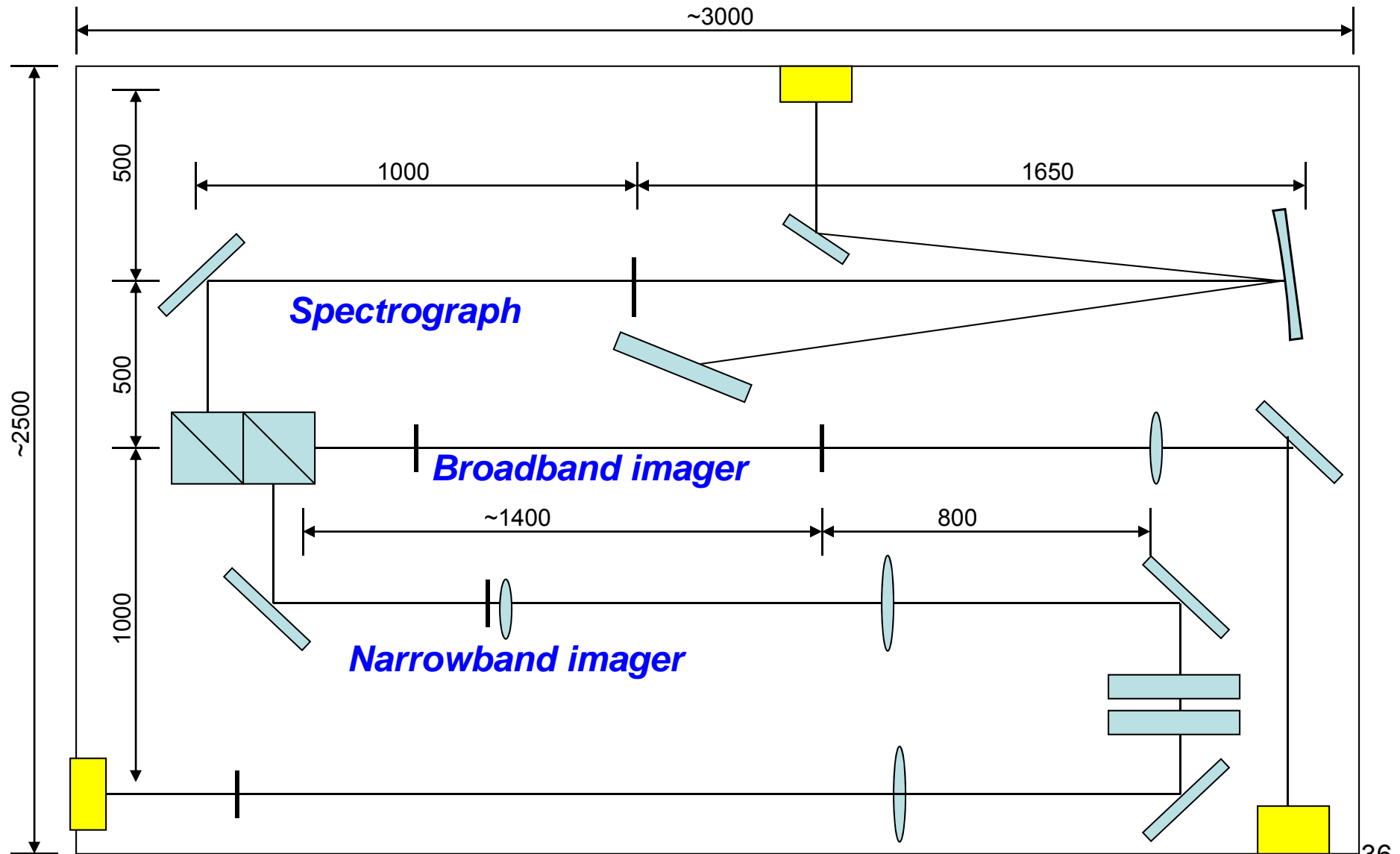
$\lambda$	Order	dispersion
2800A	73	7.0mÅ/12 $\mu$ m
8542A	24	21mÅ/12 $\mu$ m
10830	19	27mÅ/12 $\mu$ m

# Narrowband imager layout

- Telecentric configuration to have uniform wavelength over FOV.
- Large F ( $F > 150$ ) at the Fabry-Perot etalon.
- The shutter is located near the exiting-pupil.
- $0.06''/12\mu\text{m}$  pix,  $4\text{K} \times 4\text{K}$   
→  $f \sim 1650\text{mm}$  (F/28)  
→ FOV  $246''$



# Strawman layout of the focal-plane package



# Items to be further studied

- **Priority of the spectrum lines (wavelength coverage)**
  - Either spectrograph or filtergraph for each line
- Telescope thermal design
  - Radiator configuration for cooling M1
  - Development of UV-reflective and low solar absorption coating
  - Axi-symmetric vs. off-axis design
- Configuration of the narrowband filtergraph
  - Fabry-Perot or Lyot (telecentric or collimated)
- Configuration of the spectrograph
  - Multi-slit (or image slicer) or IFU (integral field unit) spectrograph to achieve high time res.
  - Multi-wavelength simultaneous obs. or multi-wavelength obs by switching filters (and tilting a grating).
- Availability of large format detectors
  - IR detector for He I 10830
  - UV enhanced detector for Mg II h/k